Effect of Conditioner Design and Polisher Kinematics on Fluid Flow Characteristics during CMP



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Problem Statement and Objective

- Fluid dynamics in CMP is really complicated Too many rotating and oscillating parts – And groove designs.
- This complexity gets exacerbated with in-situ conditioning.
- This complexity gets further exacerbated when discs of varying designs are employed.
- Current CFD and other numerical simulation capabilities are woefully inadequate for capturing various nuances in flow patterns.
- Today we will introduce a new experimental method based on fluorescence to help quantify flow patterns during conditioning
- We will focus on several case studies and explain our observations trends qualitatively and quantitatively:
 - ✓ Various CVD diamond disc working face designs
 - ✓ Platen velocities
- ✓ Further work is ongoing!

Mechanisms of Fluid Transport in CMP

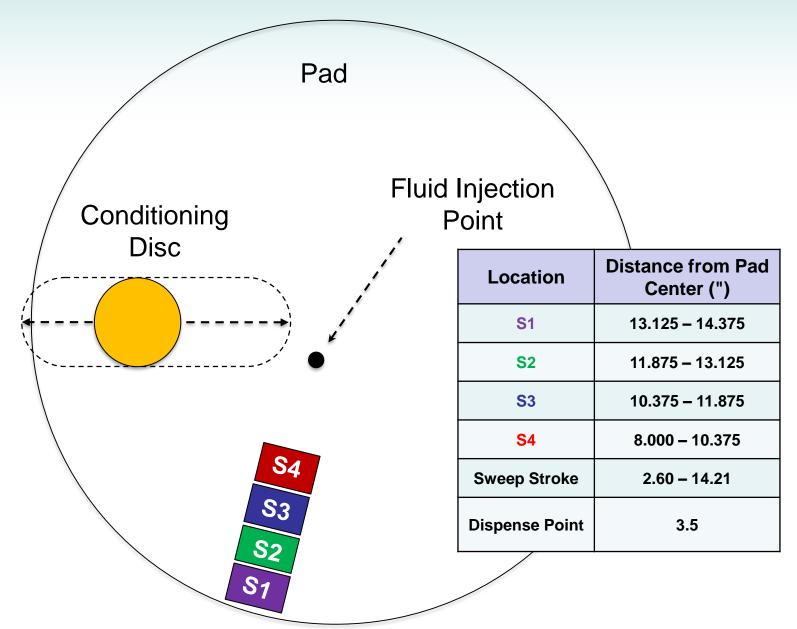
- Pad grooves, pad pores and land-area micro-texture
- Oscillatory and rotary motions of the conditioner (and the carrier head)
 - * Bow wave and boundary layer around the disc (and the retaining ring)
 - * Movement of fluid in and out of the disc-pad (and wafer-pad) interface
- Advection in the radial direction
- Centrifugal forces
- Centripetal forces mainly due to drag between pad and fluid
- Back-flow
 - Fluid build-up caused by surface tension at the edge of the pad
 - Conditioner (and wafer carrier) motion

Experimental Conditions

- Pad
 - DowDupont Politex Rotating CCW at 50 or 100 RPM.
 - Break-in 3M PB32A brush for 30 minutes at 95 RPM with platen at 50 RPM.
- Fluorescent fluid (UPW with 0.5 g/l of 4-methyl-umbelliferone) flowing at 250 cc/min with LED UV illumination
- UPW rinse at 2,000 cc/min for 30 seconds at RT between each test.

- No wafers were polished Carrier head was disengaged
- CVD Conditioners
 - * MGAM 4S
 - * MGAM 43
 - **CCW** rotation at 95 RPM
 - 3-pound down-force
 - * 11 sweeps per min
 - * 72 seconds of conditioning
- All runs were repeated once Differences in results were less than 4 percent in all cases!

Details on Various Sections Tested



The Araca UVIZ-100 System



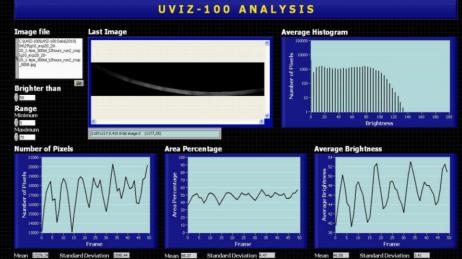
UV – LED



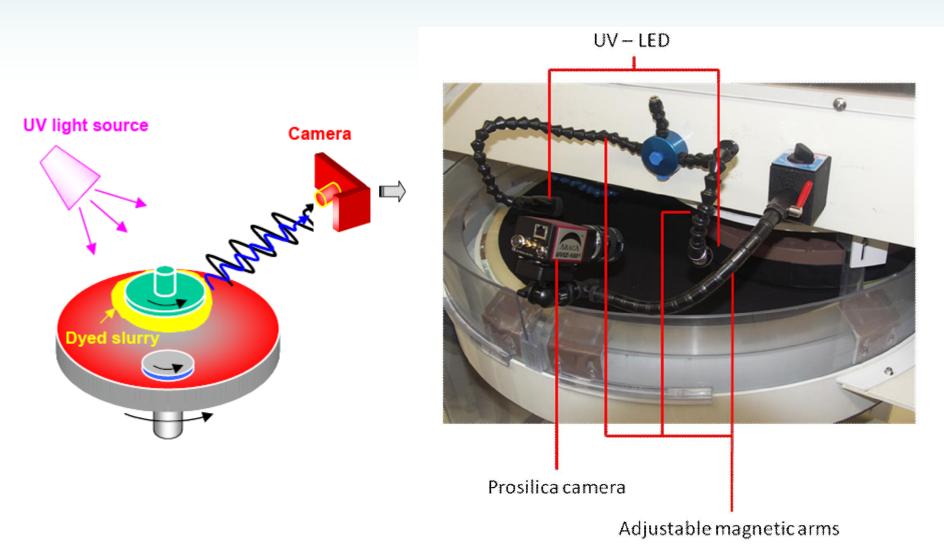
High Resolution CCD Camera

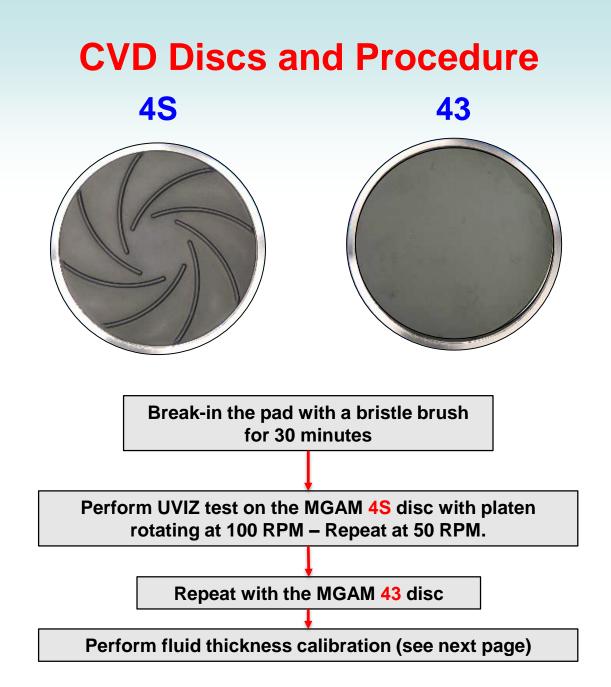


UV – LED cover

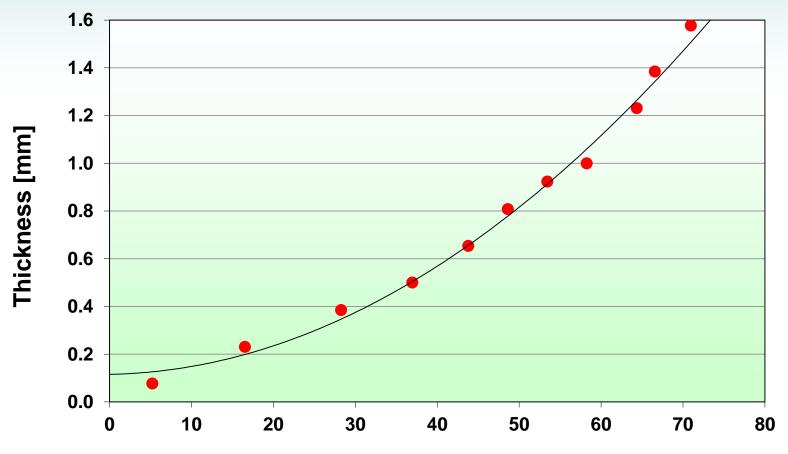


The UVIZ-100 on our APD-800 Polisher





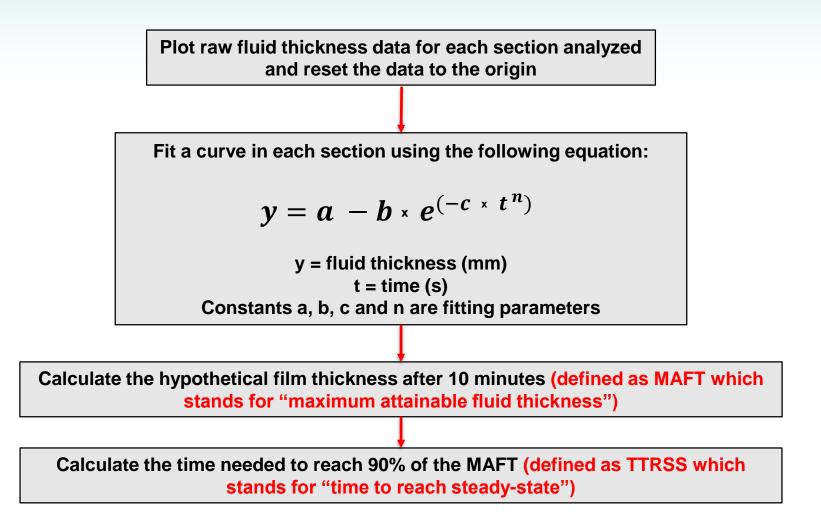
Thickness-to-Brightness Calibration Curve



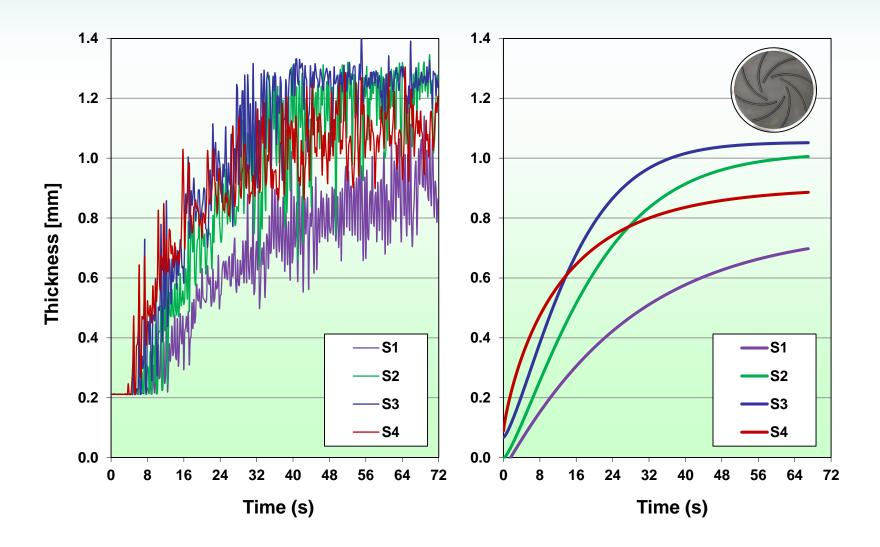
Mean Fluid Brightness due to Fluorescence

All flow visualization experiments and calibrations tests were done in a darkened room – And in 1 day so as to minimize the effect of time-dependent photobleaching.

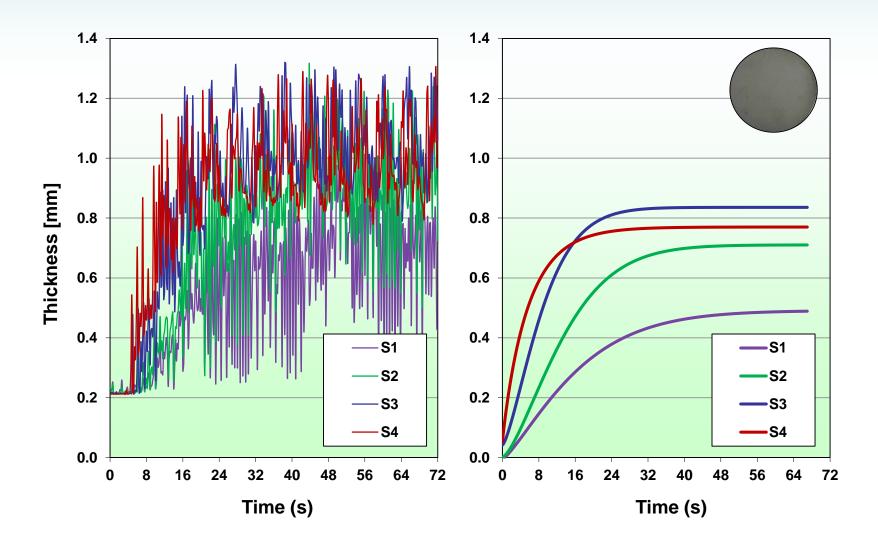
Data Analysis Flow Chart



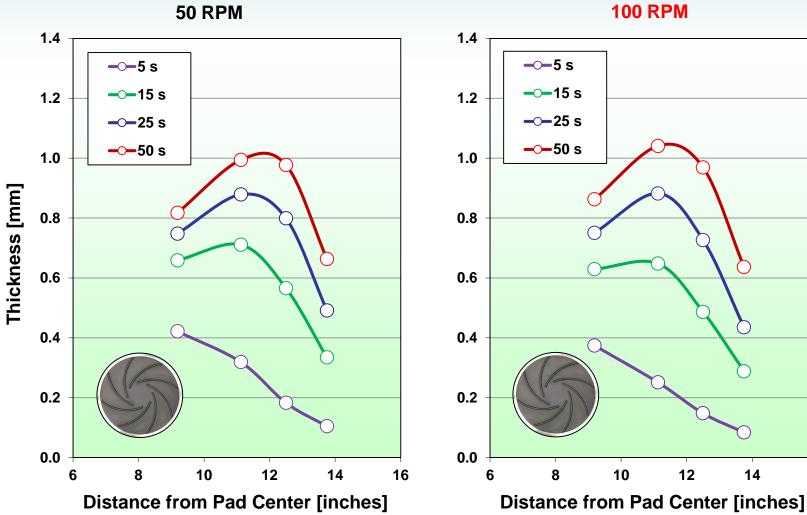
Data Analysis – 4S at 100 RPM Raw Data and Fitted Curves



Data Analysis – 43 at 100 RPM Raw Data and Fitted Curves



Disc 4S – Film Thickness vs. Distance

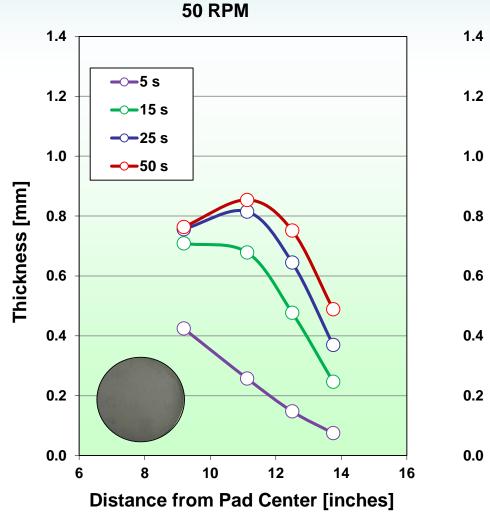


100 RPM

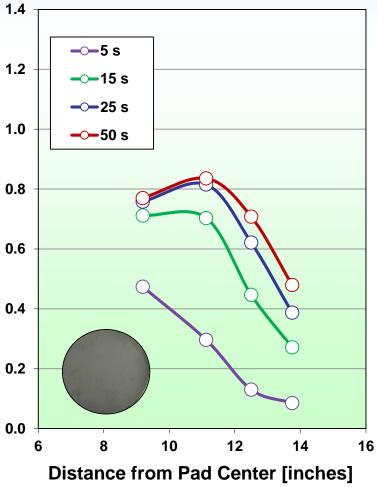
Trend Analysis

- At the shortest time, section closest to pad center has the thickest film because fresh fluid is dispensed near that region.
- At longer times, film thicknesses:
 - ✓ Closest to pad center, increase (by up to 2X) Then they level off rapidly.
 - In regions away from pad center, keep on increasing (by up to 3X) Then they level off at a slower rate. This is due to the conditioner's ability to draw fresh fluid from the center and carry it further out as it moves away.
 - ✓ Near the edge, keep on increasing (by 5X) Then they level off at a slower rate.
- Thicknesses near pad edge are lowest because fluid is removed from the surface as the conditioner moves over the edge.
- Higher pad angular velocity causes films near the edge to get thinner (due larger centrifugal forces) – No angular velocity dependence near the center.

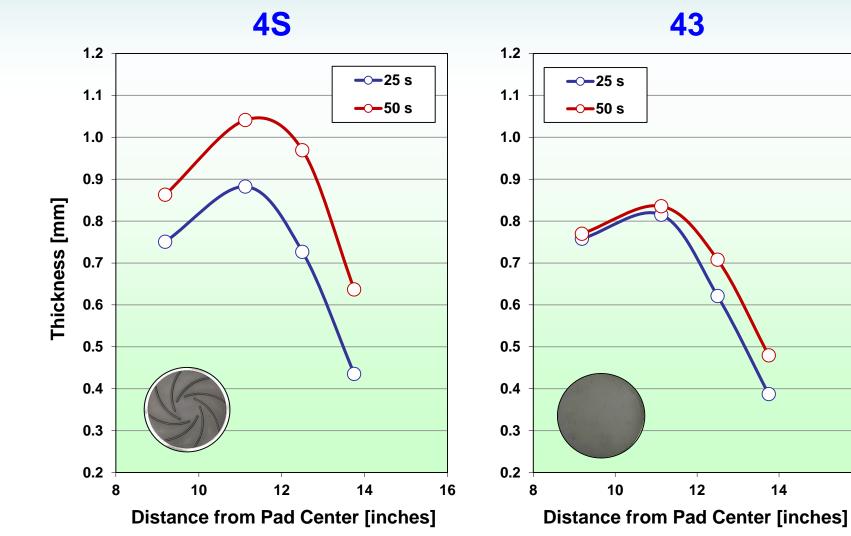
Disc 43 – Film Thickness vs. Distance



100 RPM



Disc Comparison (4S vs. 43) at 100 RPM

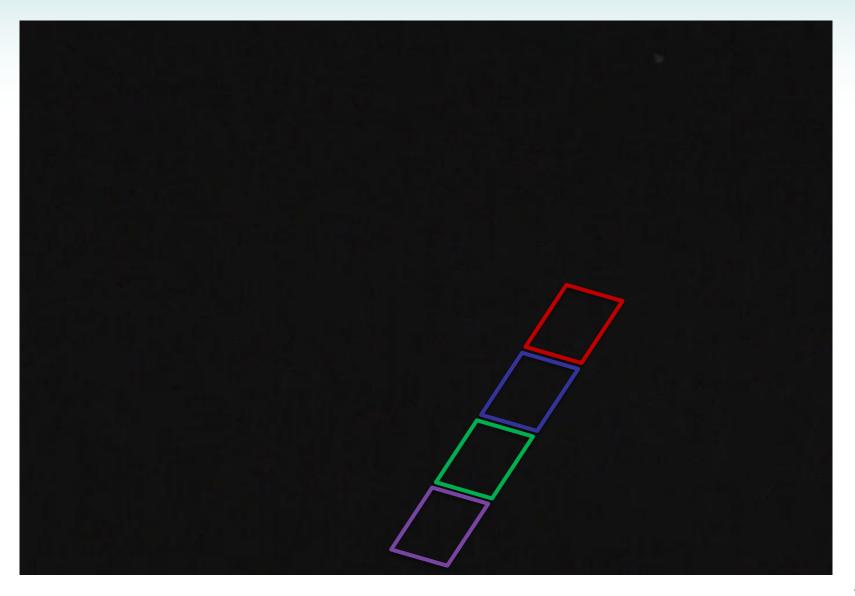




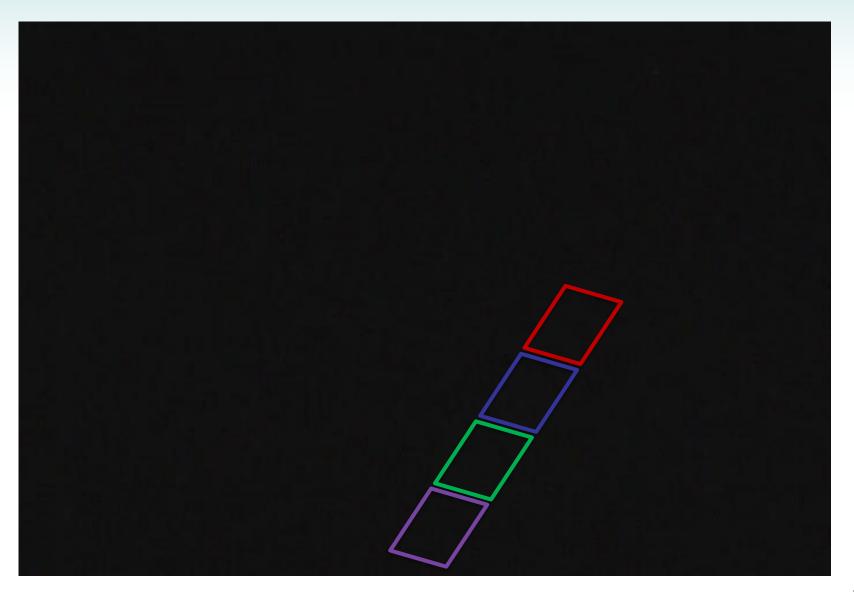
Trend Analysis

- Same general trends discussed for the 4S are apparent with the 43.
- However:
 - ✓ Full-face conditioner (43) has lower overall film thicknesses because it does not entrain fluid as effectively as the 4S which has vanes.
 - ✓ 43 tends to impart more of a squeegeeing effect and as it moves over the edge, more fluid is expelled away.
 - ✓ Due to its fluid retention characteristics, 4S generates more back-flow.
 - This effect is more pronounced at 100 RPM likely because disc rotation (95 RPM) and platen rotation (100 RPM) are nearly matched.

VIDEO – Disc 4S at 100 RPM

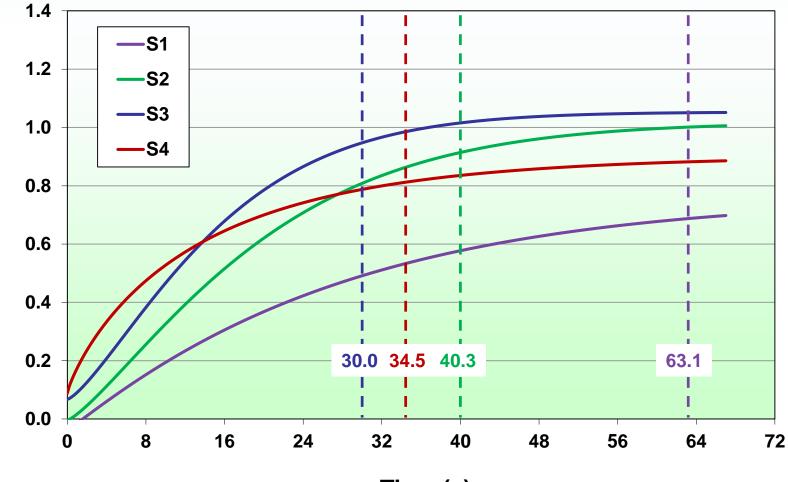


VIDEO – Disc 43 at 100 RPM



Time To Reach Steady State

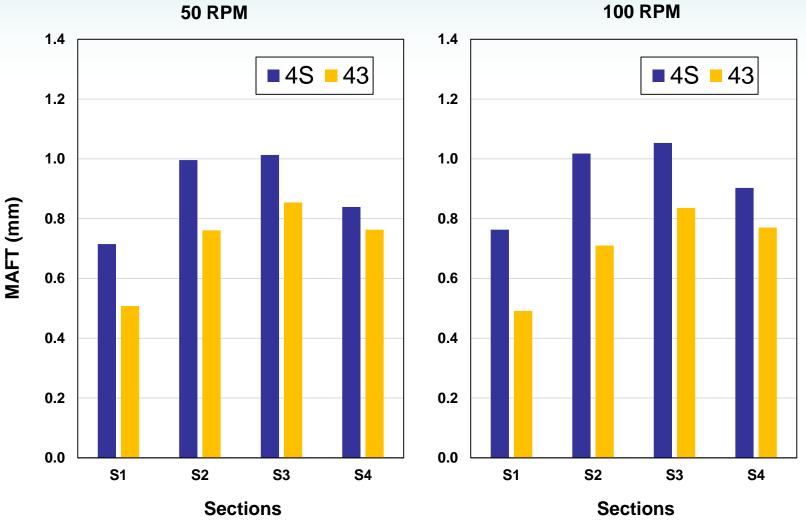
TTRSS ≡ Time needed to reach 90% of the maximum attainable fluid thickness (MAFT)



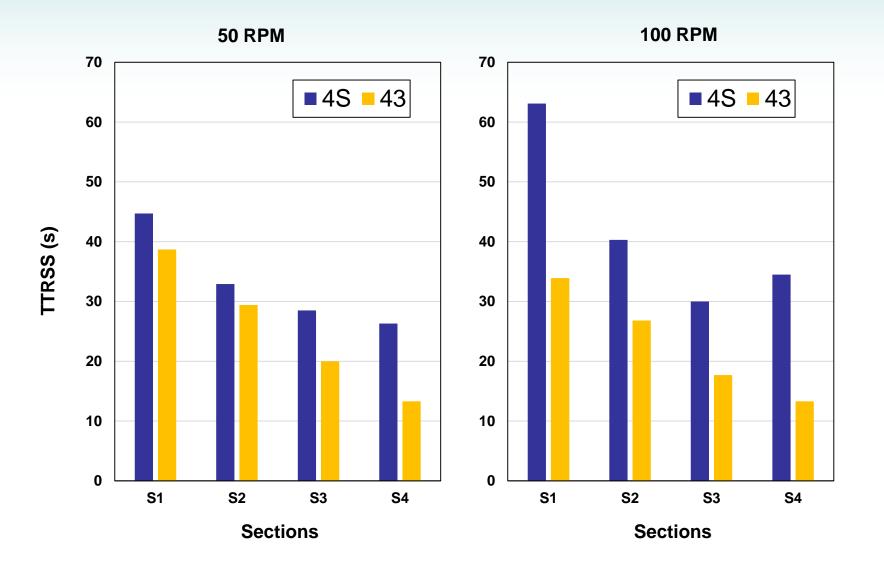
Thickness [mm]

Time (s)

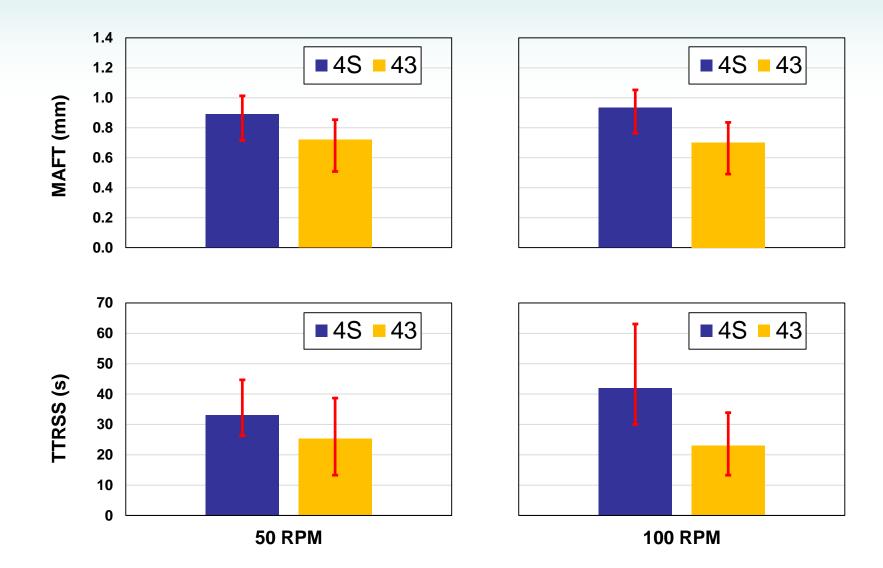
Maximum Attainable Fluid Thickness



Time To Reach Steady State



MAFT and TTRSS Means and Ranges



MAFT and TTRSS Summary

- 4S causes thicker fluid films (by 23 and 33 percent at 50 and 100 RPM, respectively) as compared to 43 – Because 4S has greater retention capabilities and generates more back-flow
- Sections near the center of the wafer track have thicker fluid
- Near the center of the pad, fluid is only slightly thinner
- Near the edge of the pad, fluid is significantly thinner
- Regarding time to reach steady-state fluid thickness conditions:
 - ✓ 4S takes longer (by 31 and 83 percent at 50 and 100 RPM, respectively) compared to
 43 Because 4S impedes and disrupts flow more effectively
 - ✓ The farther away from the pad center, the longer it takes for film thicknesses to reach SS due to the area dependence on radius (i.e. the ΠR² effect)!
- Further work using our novel technique is ongoing with the ultimate goal being to come up with the ideal disc face designs and process conditions!

Thank You!